"APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R001032010002-2

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Method of

E192/E382

ASSOCIATION.

Kafedra elektrovakuumnoy tekhniki Taganrogskogo

radiotekhnicheskogo instituta (Chair of Electrovacuum Technology of Taganrog Radio-

technical Institute)

SUBMITTED

October 12, 1959 (initially)

November 16 1959 (after revision)

Card 12/13

S/109/60/005/010/004/031 E033/E415

9,4210

AUTHOR: Malyshev, V.A.

TITLE: On the Theory of the Magnetron Oscillator

PERIODICAL: Radiotekhnika i elektrinika, 1960, Vol.5, No.10,

pp.1603-1613

There is considerable difficulty in deriving a TEXT: mathematical description of magnetron behaviour but, nevertheless, development of a complete theory of the magnetron oscillator is a V.N.Shevchik's theory of "cascare grouping" real requirement. (Ref.1) was an advance but his expressions for the electron conductance took the form of finite sums and, although it was possible to find from them a number of the oscillator parameters, nevertheless a full analysis could not be made. In this article an attempt is made, by simplifying Shevchik's formulae, to obtain a theory for the magnetron (for small amplitudes) similar in type to the theory developed by S.D.Gvozdover for the reflex klystron The article is in four sections: 1) derivation of an expression for the electron aumittance; 2) obtaining of an expression for the electron inter-action coefficient; 3) analysis of the electron admittance expression to find the regions of Card 1/6

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On the Theory of the Magnetron ...

oscillations; 4) analysis of the oscillator operation. The results obtained may be used for evaluating the effect of various specific factors on the output parameters (power, frequency). Shevchik showed that in an N-segment magnetron where each electron of the stream interacts with m slots, the real and reactive components of the first harmonic of current induced in the gap of each segment is determined by the expression

$$\begin{split} i_{a} &= 2 \frac{I_{0}}{N} M \sum_{2}^{m} J_{1} (C_{k} X_{01}) \sin \left[(k-1) (\Theta_{0} - \alpha) - D_{k} \right], \\ i_{r} &= 2 \frac{I_{0}}{N} M \sum_{2}^{m} J_{1} (C_{k} X_{01}) \cos \left[(k-1) (\Theta_{0} - \alpha) - D_{k} \right], \end{split}$$
(1)

where M is the electron inter-action coefficient; $\theta_0 = \omega \ell / v_0$ is the mean flight angle between cavities (ℓ is the distance between the gap centres, v_0 is the undisturbed electron velocity, ω is the frequency); α is the phase change between oscillations in neighbouring resonators ($\alpha = n(2\pi/N)$) where Card 2/6

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On the Theory of the Magnetron ...

n is the mode number of the oscillation: for the π -mode, $lpha=\pi$); I $_o$ is the magnetron anode current. Also

$$C_k = \sqrt{A_k^2 + B_k^2}; \quad D_k = \text{arc tg } \frac{B_k}{A_k}; \tag{2}$$

$$A_{k} = \sum_{n=0}^{k-3} (k-n-1) \cos n \, (\Theta_{0} - \alpha); \quad B_{k} = \sum_{n=0}^{k-2} (k-n-1) \sin n \, (\Theta_{0} - \alpha). \tag{3}$$

Xol is the grouping parameter in the space between the gaps.

$$x_{o1} = \frac{M\Theta_{o}}{2U_{o}} \quad U \tag{4}$$

where Uo is the potential which determines the undisturbed electron velocity; U is the a.c. voltage amplitude in the gap. The space charge is taken into account by multiplying the kinematic grouping parameter (Eq.(4)) by the factor Card 3/6

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On the Theory of the Magnetron ...

 $P = \frac{\sin\frac{l\omega_p}{v_0}}{\frac{l\omega_p}{v_0}},\tag{5}$

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where ω_0 is the plasma frequency determined by

$$\omega_{\rm p} = \sqrt{\left| 4\pi \frac{e}{m} \rho_{\rm o} \right|} = 1.83 \cdot 10^{10} \sqrt{\frac{I_{\rm o}}{NF \sqrt{U_{\rm o}}}} \tag{6}$$

F is the cross-sectional area of the stream (F = h, where h is the height of the block). The magnetron electron admittance Y_e is given by NY_{el} where

$$Y_{e1} = \frac{I_0 M^2 \Theta_0 PL}{U_0 N_T^2} \frac{J_1 (AU)}{AU} e^{-j(\delta + \pi)}, \tag{12}$$

in which

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On the Theory of the Magnetron ...

 $\delta = \tau - \frac{3\pi}{2} - \operatorname{arc} \operatorname{tg} \frac{2 \cos z\tau + (z+1) \tau \sin z\tau - z\tau^{2} - 2}{2 \sin z\tau - (z+1) \tau \cos z\tau + \tau (1-z)},$ $L = \tau \sqrt{2(z+1)^{2} + (z\tau)^{2} + \frac{8}{\tau^{2}} - 2z \left[\frac{4}{\tau} + \tau (z+1) \right] \sin z\tau - 2 \left[\frac{4}{\tau^{2}} + 2z + 1 - z^{2} \right] \cos z\tau},$ (12a)

 $A = \frac{M\Theta_0 PB}{2U_0} = \frac{M\Theta_0 P}{2U_0} \sqrt{\frac{z^4}{4} + \left[(2+z) + \frac{2}{\tau^2} \right] \left(1 - \cos \frac{z\tau}{2} \right) - \frac{z}{\tau} \sin \frac{z\tau}{2}}, \tag{12b}$

(12B)

and z = m - 2; δ is the phase of the electron admittance; $\tau = \bigodot_0 - \alpha$ is the parameter characterizing the flight angle; P is the space charge parameter. To obtain an expression for M, the electron inter-action coefficient, two effects are considered: 1) the effect of inhomogeneity of the electric field in the direction of the electron movement and 2) the fact that the electron is acted upon by only a portion of the a.c. voltage in the gap (i.e. by the field at the edges of the gap). A rectilinear electrode configuration is assumed. The phase of the electron admittance is analysed to find the oscillation regions for various

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On the Theory of the Magnetron ... E033/E415

values of m and graphs of $L/\tau^2 = f(\tau)$ and $B = f(\tau)$ are constructed. Finally, the oscillator operation is analysed by representing the oscillator system of the magnetron by an equivalenc parallel resonant circuit. There are 7 figures and 8 Soviet references.

SUBMITTED: December 14, 1959

Card 6/6

MALYSHEV, V. A., Cand Phys-Math Sci -- "solution of certain problems of the theory of oscillations for narrow-banded generators of ultra-high frequencies." Taganrog, 1961.

(Min of Higher and Sec Spec Ed RSFSR. Saratov Order of Labor Red Banner State U im N. G. Chernyshevskiy) (KL, 8-61, 1927)

- 26 -

9.3260 (1139,1159)

34258 \$/142/61/004/005/001/014 E192/E382

AUTHOR: Malyshev, V.A.

TITLE:

Influence of a small sinusoidal signal on a narrowband oscillatory system with delayed feedback

Izvestiya vysshikh uchebnykh zavedeniy, PERIODICAL: Radiotekhnika, v. 4, no. 5, 1961, 513 - 534

The problem of the influence of a harmonic signal on TEXT: a narrow-band oscillatory system with an arbitrary phase of the negative admittance is of some practical interest. this problem is solved by the method of slowly-changing amplitudes. For the purpose of analysis, it is assumed that the frequency of the external signal is near to the frameway of the free oscillations of the system and that the amplitude of the signal is small. The equivalent circuit of the my common therefore be represented as shown in Fig. In, where the parameters R, L and C characterize the oscillatory concern of the system; R_{i} is the internal resistance of the oscill that

N) is the nonlinear element of the oscillator and the Card 1/6

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lafluence of

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current $i_H = f_0(U)$, where U is the voltage across the linear element. By assuming that $i = i_0 + i_H$ and $i_0 = U + E_0^2 \cos \beta t$. the system is described by the following equation:

$$\frac{d^{2}U}{d\tau^{2}} + U = hU - \frac{1}{Q} \frac{dU}{d\tau} + E \sin \approx -\frac{1}{C\omega_{o}} \frac{di_{H}}{d\tau}$$
 (1)

where $\tau = \omega t$, $h = 1 - \omega_0^2/\omega^2 \simeq 2 \Delta \omega/\omega_0$, Q is the quality factor of the resonance circuit, $\omega_0^2 LC = 1$, $Q_B = \omega_0^2 CR_1$ is the quality factor of the resonance circuit with load and $E_o = ER_i C\omega \simeq EQ_B$, $Q = C\omega_o RR_i / (R = R_i) \simeq C\omega_o RR_i / (R + R_i)$ Since the righthand-side portion of Eq. (1) is smaller than each of the terms in the lefthand-side portion, the solution of Eq. (1) is in the form of:

 $U = A(\tau)\cos[(\tau - \Theta(\tau)] = A\cos\alpha$ (2)

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(3)

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where $\lambda(\tau)$ and $\Theta(\tau)$ are slowly changing functions of time. is shown that the simplified equations for A and Θ are in the form $\frac{dA}{d\tau} = -\frac{1}{2\pi} \int_{0}^{2\pi} [hA\cos\alpha + \frac{1}{Q}A\sin\alpha + E\sin(\alpha + \Theta)] \sin\alpha d\alpha + \frac{1}{2\pi C\omega_0} \int_{0}^{2\pi} \frac{dt_{\pi}}{d\tau} \sin\alpha d\alpha;$

 $\frac{d\Theta}{d\tau} = \frac{1}{2\pi A} \int_{0}^{2\pi} \left[hA \cos \alpha + \frac{1}{Q} A \sin \alpha + E \sin (\alpha + \Theta) \right] \cos \alpha \cdot d\alpha - \frac{1}{Q} + \frac{1}{Q} \sin \alpha +$

 $-\frac{i}{2\pi C\omega_0 A}\int\limits_0^{2\pi}\frac{d\ell_n}{d\tau}\cos\alpha d\alpha.$

where F is the amplitude of the first current harmonic, which is, in general, dependent not only on A but also on the frequency ω ; t is the phase difference between the first harmonic of the current i_H and voltage U and the angle π (δ is often referred to as the phase or the negative admittance of the oscillator). In general, the quantities F and δ can be determined by the method indicated in Ref.7 (Izv. vuzov SSSR - Radiotekhnika, 1960,v.3, no.5, 474) by using:

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Influence of ...

$$F(A)e^{-l(\delta+\pi)} = \frac{2l}{T} \int_{0}^{T} e^{-l\omega t} f_{\mathbf{0}}(A\sin\omega t) dt.$$

It is also shown (Ref. 6 - I.M.Kapchinskiy - Methods of the theory of oscillations in radio-engineering - Gosenergoizdat, 1954) that the conditions of stable operation of the system at the frequency ω are determined by

$$P = -\left(\frac{\partial \Phi}{\partial A} + \frac{\partial \Psi}{\partial \Theta}\right) > 0; \quad q = \left(\frac{\partial \Phi}{\partial A} \cdot \frac{\partial \Psi}{\partial \Theta} - \frac{\partial \Phi}{\partial \Theta} \cdot \frac{\partial \Psi}{\partial A}\right) > 0. \tag{6}$$

The above expressions are employed to investigate the general case of the oscillators with weak excitation, in which $\delta \neq f/(A)$, $\delta \neq f(\omega)$, and $F \neq f(\omega)$. The formulae derived are then used to study the pull-in of a vacuum-tube oscillator and that of UHF oscillators. The case of under-excited oscillators (regenerative amplifiers) of the vacuum-tube and UHF types is also considered. The expressions derived for these systems were verified experimentally, in particular for UHF generators (reflex klystrons). From the analysis and experimental results, it was found that as the negative-admittance phase δ increased Card 4/6

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Influence of

from 0 to 100°, the frequency bandwidth between the half-power points of the output signal increased monotonically. As regards the regenerative and negative-feedback operation of the system, the amplitude monotonically decreased as the phase of the negative admittance varied from the value corresponding to the transition conditions to δ = 180° . When δ changes from transition conditions to 0 to 180° , the regions of instability undergo considerable changes; in particular, in the pull-in and negative-feedback regimes two regions of instability and 3 different types of unstable points are encountered; when the operating conditions correspond to the transition from regeneration to pull-in, the maximum output signal increases and the bandwidth becomes reduced as 5 changes from 0 to 90°. In vacuum-tube oscillators the highest gain in the regenerative system can be obtained for values of 5 60° , when an unstable region occurs within the amplification bandwidth. One of the important problems in the operation of a regenerative amplifier is the gain stability. The experiments show that stable operation of a reflex klystron amplifier can be achieved by employing the usual electronic stabilizers and that a stable gain of 20 db can be obtained. Card 5/6

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Influence of

There are 11 figures and 18 references: 17 Soviet-bloc and 1 non-Soviet-bloc. The English-language reference mentioned is: Rer. 18 - M. Chodorow and V. Westburg - PIRE, 1951, 39, no. 12, 1548.

ASSOCIATION:

Kafedra obshchey fiziki Rostovskogo-na-Donu

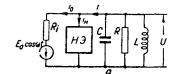
gos. universiteta (Department of General Physics

of Rostov-on-Don State University)

SUBMITTED:

May 11, 1960

Fig. la:



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9,4230 (also 1532)

S/109/61/006/003/003/018 E140/E135

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Malyshev, V.A., and Mikhalevskiy, V.S.

TITLE:

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On the Theory of the TWT-Oscillator With Weak Feedback

PERIODICAL: Radiotekhnika i elektronika, 1961, Vol.6, No.3,

pp. 363-370

In previous work the problem of the title has been TEXT: treated only qualitatively. The present article attempts to derive certain features of operation of such oscillators using the cinematic approximation. The detailed mechanism for realization of feedback is not considered, it being assumed only that the feedback factor for a given space harmonic is much less than unity and independent of the generated frequency which must be close to one of the natural frequencies of the system. These conditions are best realized in oscillators with external feedback; oscillators with internal feedback they can be satisfied only under the condition of negligibly small interaction of the modulated electron stream with the reflected wave. These conditions are not satisfied in reflex TWT. The delay system is considered in the form of a simple resonator with natural frequencies fairly closely Card 1/6

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On the Theory of the TWT-Oscillator With Weak Feedback

spaced. It is assumed that measures have been adopted on the device for separation of the natural frequencies, for example by the use of a special filter in the feedback circuit, or by the use of systems with normal dispersion. This assumption permits neglect of the possibility of oscillation at several neighbouring frequencies. Finally, the analysis takes into account interaction of the flow only with a single definite space harmonic of the wave, uniquely defined by the phase velocity in the system. The analysis proceeds from the equation of motion of the electron, from which the Kepler's equation for the transit angle of the electron has been found by V.N. Shevchik (Ref. 10):

$$\varphi = \varphi_0 - \frac{\mu e^{\frac{\gamma v_{\infty}}{\omega}}}{\rho \left(1 + \frac{\gamma t_0}{\theta 1}\right)} \sin \left(\omega t - \frac{v_0}{v_{\phi}} \varphi - \psi\right), \tag{3}$$

where:

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ion the Theory of the TWT-Oscillator With Weak Feedback

$$tg \psi = \frac{1 - \frac{\gamma^{0}}{\theta^{0}}}{2 \frac{\gamma}{\theta}}; \quad \theta = \frac{\omega}{v_{0}} \rho = \frac{\omega}{v_{0}} \left(1 - \frac{v_{0}}{v_{\phi}}\right); \quad \mu = \frac{aB_{1}}{mv_{0}\omega \left(1 - \frac{v_{0}}{v_{\phi}}\right)}; \quad (4)$$

 $\varphi = \omega t - \omega \tau; \ \varphi_0 = \frac{\omega x}{v_0},$

where: τ - time of electron entry into the system; γ - propagation constant; ε - the electron charge; v_0 - the phase velocity of the wave; v_0 - the velocity of the undisturbed electron. Examining further the interactions taking place in the system, an equivalent circuit is found (no diagram given) in the form of a parallel combination of L, C, G and G₁ elements, where G₁ represents the load losses and G the device losses. Then the electron stream represents a conductance for which there is given the expression

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On the Theory of the TWT-Oscillator With Weak Feedback

$$Y_e = 2G_0 \frac{1 - J_0(X)}{X^2} e^{-j(8+\pi)} = G_e + jB_e$$

where
$$G_{0} = \frac{9\epsilon\omega I_{0}}{\gamma m M^{3} v_{0}^{3} (\theta^{3} + \gamma^{3})} = pI_{0}; \quad X = \frac{3\epsilon\omega U}{m M v_{\phi} v_{0}^{2} (\theta^{3} + \gamma^{3})} = rU;$$

$$\delta = \psi - \pi = \text{arc tg} \frac{\theta^{3} - \gamma^{3}}{r} - \pi.$$

$$\delta = \psi - \pi = \operatorname{arc} \operatorname{tg} \frac{\theta^{3} - \gamma^{3}}{2\gamma\theta} - \pi.$$

where X is the bunching parameter. Based on these relations, the author then analyzes the operation of the oscillator, determining the output power and frequency of oscillation. particular the question of electronic tuning is considered and approximate expression found for the whole range of $\triangle \omega_{\mathbf{p}}$

$$\Delta\omega_{p} = \frac{\sqrt{1-4N^{2}v_{0}^{2}\gamma^{2}}}{N\left|\left(B\omega_{0}v_{\Phi} + \frac{\gamma}{\beta_{0}}\right)\right|}; \qquad \beta_{0} = \frac{\omega_{0}}{v_{\Phi}},$$

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On the Theory of the TWT-Oscillator With Weak Feedback

$$\left(\frac{\partial v_{\Phi}}{\partial \omega}\right)_{0} = -\frac{4Q_{H}\gamma v_{\Phi}^{2} \left(1 - \frac{1}{2Q_{H}}\right)^{2}}{\omega_{0}^{2} \left(2 - \frac{1}{Q_{H}}\right)} \simeq -\frac{2Q_{H}\gamma v_{\Phi}^{2}}{\omega_{0}^{2}} = -\frac{Q_{H}\gamma \lambda^{2}}{2\pi^{2}} \left(\frac{v_{\Phi}}{c}\right)^{2}, \tag{21}$$

where γ and c - wave length and speed of light in the free space. Finally optimal loading for a given value of X

$$\frac{J_{1}(x)}{x} = \frac{G}{G_{0} \cos \delta}; \quad \frac{1}{x} \left[\frac{1 - J_{0}(x)}{x} - J_{1}(x) \right] = \frac{G_{H}}{G_{0} \cos \delta} \quad (26)$$

The oscillator efficiency, time of establishment and load characteristics are also discussed. The authors' conclusion Card 5/6

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On the Theory of the TWT-Oscillator With Weak Feedback

that a system with normal dispersion leads to stable wide-band operation contradicts the conclusion of E. Jones (Proc. I.R.E., 1952, 40, 4, 478) (Ref.1) and M. Denis (Ann. radioelectr., 1952, 7, 29, 169) (Ref.2), that systems with anomalous dispersion should be superior. This is due to the fact that these authors in their analysis completely ignored the reactance of the electron stream. The present work is in accordance with experimental results and is analogous in character to well-established formulae in the theory of the reflex klystron.

There are 3 figures and 14 references: 10 Soviet and 4 non-Soviet.

SUBMITTED: June 27, 1960

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22898

\$/109/61/006/004/012/025 E140/E135

9,2585 **AUTHOR:**

Malyshev, V.A.

TITLE:

On the theory of _ode microwave oscillators

PERIODICAL: Radiotekhnika i elektronika, Vol.6, No.4, 1961,

pp. 604-612

TEXT: Analysis of retarding-field diode oscillators shows that they have no substantial advantages over reflex klystrons, either in regard to the range of electronic tuning or maximum An increase in the rate of electronic tuning (by a factor of 1.42) is balanced by a commensurate deterioration in the frequency stability. The obtained results show that the operation of diode oscillators is generally similar to the operation of reflex klystrons and that all the types of diode oscillators considered in the paper can be studied and calculated in the same way. The output parameters of diodes with a retarding field may be close to the values observed in analogous reflex klystrons. The analysis given in this paper confirms experimental results published by C.J. Carter, W.H. Cornett and

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On the theory of diode microwave oscillators

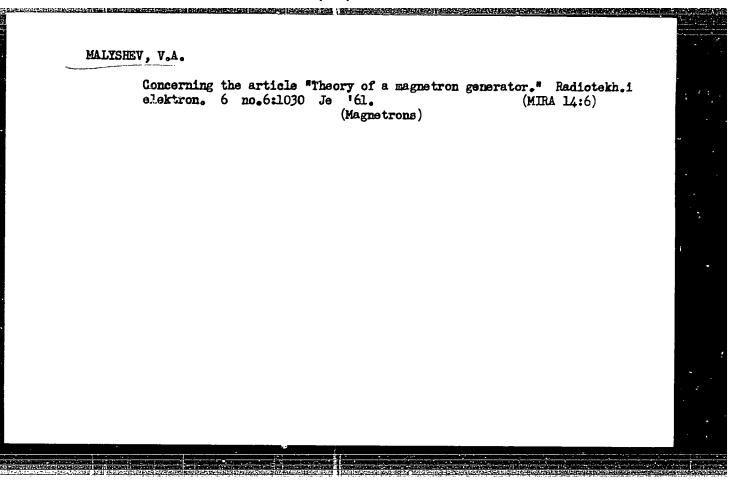
M.O. Thurston (Ref.7: Vide, 1956, Vol.12, 65, 281).

There are 4 figures and 10 references: 6 Soviet, 3 English and 1 translation from English into Russian.

SUBMITTED: February 15, 1960

Card 2/2

"APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R001032010002-2



S/057/61/031/002/007/015 B020/B067

26.2351

AUTHOR:

Malyshey, V. A.

TITLE:

Kinetics of the pumping of vacuum systems in quasisteady

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state

PERIODICAL: Zhurnal tekhnicheskoy fiziki, v. 31, no. 2, 1961, 200-203

TEXT: The published theoretical data on the pressure change with time in an evacuated vacuum system are based on the assumption that the rate of evacuation of the pump is independent of pressure but depends on the quasisteady state during the evacuation. The effective rate of evacuation in a real vacuum system depends, however, on the pressure in the system. Taking account of this dependence the kinetics of the evacuation process in the real vacuum systems can be determined more exactly. The present paper deals with this problem. All conditions are assumed to be fulfilled which are necessary to attain the quasisteady state. Sp and S are the

effective rates of evacuation of the pump and the vacuum system, S_p^i and S^i the actual rates of evacuation of the pump, p_1 is the initial pressure in

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Kinetics of the pumping of ...

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the vacuum system and simultaneously also the pressure in the exhaust tube of the pump and po the limiting pressure attained by means of the pump. The limiting pressure is explained by a backflow of the gas from the pump into the system. In mechanic pumps this backflow has the same character as the passage of a gas through a small opening whose permeability K is independent of pressure. The backflow $K(p_1-p')$ increases with decreasing

pressure. The resulting gas flow is given by $S_p p^i = S_p^i p^j - K(p_i - p^i)$, where p' denotes the pressure at the suction tube of the pump, if

 $p' = p_1$, $S_p = S_p'$, with $p' = p_0$, however, $S_p = 0$ and

(1)

 $S_p^i = K^i(p_1 - p_0/p_0); Kp_1 = p_0(S_p^i + K)$ and with $C = S_p^i + K = K^{p_1/p_0}$ the author obtains $S_p = C(1-p_0/p^i)$

The relation obtained between the pressures at the ends of the tubes is

$$p - p_0 = \frac{C + U}{U} (p' - p_0);$$
 (5)

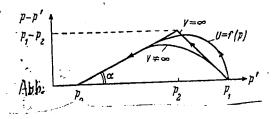
$$p - p' = \frac{C}{U}(p' - p_0). \tag{6}$$

Kinetics of the pumping of ...

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is obtained as the dependence of the pressure drop at the ends of the tubes on pressure p' at the pump. Equation (6) does not hold: in the region of the initial pressures. This is explained by the fact that the flow along the tube is not constant and the conditions are quasisteady. The pressure region $\mathbf{p_1} - \mathbf{p_2} = (\mathbf{C}/\mathbf{C} + \mathbf{U})(\mathbf{p_1} - \mathbf{p_0})$ at the suction tube of the

pump is the region of quasisteady conditions for the ideal case of an infinitely large volume (V) of the sucked-off object. The general dependence of the pressure difference at the ends of the tube on pressure p' is shown in the Fig.



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Kinetics of the pumping of ...

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(the direction of the change of function p-p'=f(p') with time being indicated by arrows). The relations obtained can be practically applied. Equation (6) indicates that in the absence of negative sources pressure drop at the ends of the tube becomes zero. This is an advantageous criterion when examining the tightness of the system. Practical experiments were made with a vapor-oil pressure pump $C\Delta H - 1$ (SDN-1) in a pressure region in which the conditions of evacuation can be regarded as steady, whereas the conditions of air flow are molecular. The evacuation kinetics are determined by equation (8)

taking account of the backflow into the object, where V is the volume of the sucked-off object. There are 1 figure and 3 Soviet-bloc references.

ASSOCIATION: Taganrogskiy radiotekhnicheskiy institut (Taganrog Radiotekhnicheskiy institut (Taganrog Radiotekhnicheskiy institut)

SUBMITTED: October 16, 1959

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5/141/62/005/001/013/024 E203/E435

9 4110

Malyshev, V.d. AUTHOR:

Theory of plate diode with a uniform cathode under TITLE:

saturation conditions

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Radiofizika.

v.5, no.1, 1962, 128-135

This paper was presented at the Conference of MV and SSO SSSR on Radioelectronics, Khar'kov, 1961 and at the TEXT:

7th Scientific-Technical Conference of the Taganrog Radioengineering

A quantitative evaluation is made of the effect of the space charge on the current-voltage characteristic of a plate diode (without spots and non-uniformities) a d the consequent deviation From energy considerations the author from Schottky's law. derives formulae for a correction coefficient γ in respect of the nonuniformity of the field between the electrodes and for a dimensionless parameter C depending on the work function of the cathode material, the distance between the electrodes and the A few actual values of C are quoted for the more temperature. Card 1/3

S/141/62/005/001/013/024 E203/E435

Theory of plate diode ...

The following conclusions are drawn. common cathode materials. The space charge influence can only be neglected at such high anode potentials which often cannot be realized in practice or demand power dissipation beyond the anode's capability. more usual conditions practical errors result, for instance an extrapolation of the current-voltage curve down to zero field values will always result in too low a figure for emission current Richardson's method for determining emissivity and work function will give values too low for both. The author then gives a detailed method of solving the problem graphically, obtaining near approximations to actual conditions. calculations having been based on the assumption of a uniform smooth cathode, two criteria arise to test this assumption. The experimental and theoretical values of C must coincide; the slope of the current-voltage characteristic must follow the It is claimed that non fulfilment of "three halves power law". these criteria gives a measure of the non-uniformity of the The author points out that errors arise due to finite dimensions of the diode and that these errors will increase, Card 2/3

"APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R001032010002-2

Theory of plate diode ...

S/141/62/005/001/013/024 E203/E435

decreasing diode dimensions and increasing current density. There are 3 figures and 2 tables.

ASSOCIATION: Taganrogskiy radiotekhnicheskiy institut

(Taganrog Radioengineering Institute)

SUBMITTED: April 15, 1961

B

Card 3/3

26 Y358

\$/057/62/032/003/014/019 B139/B102

AUTHOR:

Malyshev, V. A.

TITLE:

Effect of sorption on kinetics of evacuation of vacuum

PERIODICAL: Zhurnal tekhnicheskoy fiziki, v. 32, no. 3, 1962, 360-364

TLXT: The author develops the kinetic equation of the evacuation of vacuum systems for quasi-steady conditions in the light of a sorption which proceeds proportionally to pressure, and analyzes the effect of sorption on the evacuation parameters. If the sorption isotherm satisfies Henry's law, it follows that $\left(\frac{dn}{dt}\right)_g = \beta \left[\frac{f(p)}{\sqrt{1-p}} - n\right]$, where n is the molecular

concentration on the walls, describes the diffusion through the

walls, β is a definite coefficient, f(p) is the adsorption per unit area, v is the evaporation probability of a surface molecule per unit time. Desorption is characterized by the relation

Card 1/3

S/057/62/032/003/014/019 B139/B102

Effect of sorption on kinetics...

 $\left(\frac{dn}{dt}\right)_{x} = -\left(\frac{dn}{dt}\right)_{x} = vn - ap$. Hence the gas afflux to the system per second

 $\frac{dN}{dt} = k^m q (Nn - ap)$ where q is the wall area of the system. The pressure ratio is given by

 $x + 2\beta x + \omega_o^2 x = 0$ where $x = p - p_f$; $\beta = \frac{Y}{2V}(C + kTqa) + \frac{v+3}{2}$; $\omega_o^2 = \frac{C\gamma v}{V} \left[1 + \frac{\rho}{v}\right]$

Since $p^2 > \omega_0^2$ is satisfied in any case and the conditions at the onset of evacuation always guarantee the inequalities $x_0 < 0$; $-x_0 = (2 + \sqrt{2} - \omega_0^2)x_0$ (17) the solution of (13) represents a monotonically decreasing function. The

dependence $-\ln \frac{p - p_f}{p_{in} - p_f} = f(t)$ is represented by a straight line of the slope $\frac{\partial Y}{Y}$ toward the time axis(dashed line in Fig. 1); in the case of large t, the slope may come up to P - σ (full line in Fig. 1). Owing to

Card 2/3

"APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R001032010002-2

Effect of sorption on kinetics...

S/057/62/032/003/014/019 E139/B102

sorption, the slope of the curve indicated by the full line toward the dished curve decreases during evacuation thus indicating decreasing evacuation rate. Sorption is most distinct at small time constants $\frac{V}{VC}$ and low temperatures. There are 2 figures and 5 references: 3 Soviet and 2 non-Soviet.

ASSOCIATION: Taganrogskiy radiotekhnicheskiy institut (Taganrog Institute

of Hadio Engineering)

SUBMITTED: April 17, 1961

Card 3/3

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"APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R001032010002-2

S/057/62/032/012/011/017 B104/B166

AUTHOR:

Malyshev, V. A.

TITLE:

Symmetrical stationary problem of isothermic gas diffusion

PERIODICAL: Zhurnal tekhnicheskoy riziki, v. 32, no. 12, 1962, 1482-1483

TEXT: The stationary solution of the total differential equations

$$D_{\nu}\nabla^{2}(\ln\nu) = \frac{\partial\nu}{\partial r}$$
.

(4)

 $D_0 = \nu D = \frac{2T}{3\pi z^2 (T+C)} \sqrt{\frac{kT}{\pi m}}.$

describing the isothermic diffusion of a single-component gas is studied. $D = \frac{1}{3} v\lambda; \qquad v = \sqrt{\frac{8kT}{\pi m}}; \qquad \lambda = \frac{1}{\sqrt{2} \pi \sigma^2 v(1 + \frac{C}{T})}$

$$D = \frac{1}{3} v\lambda;$$

holds for the diffusion coefficient, where m is the mass of the molecule,

Card 1/3

APPROVED FOR RELEASE: 06/20/2000

CIA-RDP86-00513R001032010002-2"

Symmetrical stationary problem...

C the Sutherland constant, σ the diameter of the molecule, ν the concentration. If the boundary conditions are $\frac{1}{x=x_1} = \frac{\nu}{1}$ and $\frac{\nu}{x=x_2} = \frac{\nu}{2}$ and

the diffusion is one-dimensional the stationary solution of (4) can be written in the form

$$v = v_{l_1}^{\frac{x_1 - x}{x_1 - x_1}} v_{2}^{\frac{x - x_1}{x_1 - x_1}}.$$
 (6).

For the gas flow through the unit cross-section

$$Q = -D_0 \frac{d (\ln v)}{dx} = \frac{D_0}{x_2 - r_1} \ln \frac{v_1}{v_2}. \tag{7}$$

is given. If 2 is known, one of the boundary conditions can be found. The stationary solution of (4) with axially symmetrical diffusion can be given in the form

$$\mathbf{v} = \left(\mathbf{v}_{1}^{\mathrm{la}} \frac{\mathbf{r}}{r_{1}} \mathbf{v}_{3}^{\mathrm{la}} \frac{\mathbf{r}_{1}}{r_{1}}\right)^{\mathrm{la}} \frac{\mathbf{r}_{1}}{r_{3}}, \tag{8}$$

Card 2/3

Symmetrical stationary problem...

if the boundary conditions are $v|_{r=r_1} = v_1$ and if $v|_{r=r_2} = v_2$. The gas

flow through a cylindrical surface of unit length is obtained from

$$Q = -D_0 2\pi r \frac{d(\ln \nu)}{dr} = 2\pi D_0 \frac{\ln \frac{\nu_1}{\nu_2}}{\ln \frac{r_2}{r_2}}.$$
 (9).

ANA NEGANAKAN ANGANAKAN MENUANGAN KANTANTAN MENUANTAN ME

The solution of (4) for a stationary central-symmetrical diffusion takes the

$$\mathbf{v} = \left[v_1^{R_1(R_1 - R_1)} v_2^{R_2(R - R_1)} \right]^{\frac{1}{R_1(R_2 - R_1)}}, \tag{10}$$

subject also to

$$Q = -4\pi R^2 D_0 \frac{d (\ln \nu)}{dR} = \frac{4\pi D_1 R_1 R_2}{R_2 - R_1} \ln \frac{\nu_1}{\nu_2}.$$
 (11)

if the boundary conditions are analogous as above.

ASSOCIATION: Taganrogskiy radiotekhnicheskiy institut (Taganrog Radio

Engineering Institute)

March 20, 1962 (initially) June 26, 1962 (after revision) SUBMITTED: Card 3/3

<u>16211_63</u> EMT(<u>).</u> JESSION IR: AR3005176)/BDS AFFTC/ASD	s/0058/63/000/	006/8027/8027	一一次是
JRCE: RZh, Fisika, Abs.	6 2h 170		<i>5</i> [
THOR: Maly shev, V. A.			J.	
TE: Principles of calcul	ation of the complin	() g of a resonator	and a	
ensaission line				
TED SOURCE: So. Yopr. ele ganrog, 1962, 50-60	ctroniki:1 elektrodi	namiki sverkhvyl	sokikh chastot,	
PIC TAGE: coupling loop,	round loop, square	lcsp, rescustor	coupling,	
manisalon line coupling				
NSIATION: The parameters constor with a transmission	a line are calculate	d; the coupling	is assumed to b	
bictive. Assuming the part I the resonant-circuit off				
p are calculated. The us uples therein a round and	e of the theory deve	loped is illustr	ated with speci	fic
ne for the 10 cm band.	Yu. Pirogov.			
F6 ACQ: 15Ju163	SUB CODE: GE	, sp en(L: 00	

S/139/63/000/001/022/027 E202/E420

AUTHORS: Zavadovskaya, E.P., Lazebnikov, Yu.Ye., Halyshev, V.A.

TITLE: Experimental checking of the theory of frequency characteristics of photoresistors and luminophors

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Fizika,

no.1, 1963, 142-146

TEXT: The authors developed apparatus to check the two formulas

$$\frac{\dot{\phi}}{\phi} = \frac{1 - e^{\frac{1}{2} \frac{1}{2}}}{\frac{1}{2} \frac{1}{2}}; \dot{y} = 2ef;$$

$$+ e$$
(4)

$$\frac{a}{\sigma_0} = \frac{\ln\frac{1}{x}}{1 + x \ln\frac{1}{x}} \left[x - \frac{2f}{\sqrt{Na}} \right], \tag{5}$$

where Φ and Φ_{o} are the luminescence pulse amplitudes at a Card-1/3

Experimental checking ...

S/139/63/000/001/022/027 B202/B420

frequency of and zero frequency respectively; t - lifetime of an electron in an excited state, f - frequency of the square wave pulses irradiating the luminophor. N - rate of generation of the current carriers per unit volume due to the irradiation, a - probability of recombination of the current carrier in a unit volume with one of the recombination centers; σ and $\sigma_{
m o}$ amplitudes of the photoconductive pulses, oo corresponding to the zero frequency of irradiation. Eq.(4) was checked for the case of cathode luminescence of Zn2SiO4.Mn which has exponentially decaying luminescence. Cathode luminescence was studied in a 6E5C (6Ye5S) tube which was incorporated in a circuit containing a square wave pulse generator and a photoelement CLLB (STsV) with an oscilloscope. Values of au measured at a frequency of 10 cs were $(1.14\pm0.01)\cdot10^{-2}$ sec. It was shown that with the coefficient of filling $\gamma=0.5$, the decrease of frequency did not increase the amplitude of the luminescence, hence knowing T and $\Phi_{\mathbf{0}}$ it was possible to determine \mathbf{y} and $\Phi/\Phi_{\mathbf{0}}$ for each measured value of frequency. A graphical comparison showed good agreement between the experimental and theoretical results of luminescence Card 2/3

Experimental checking ...

S/139/63/000/001/022/027 E202/E420

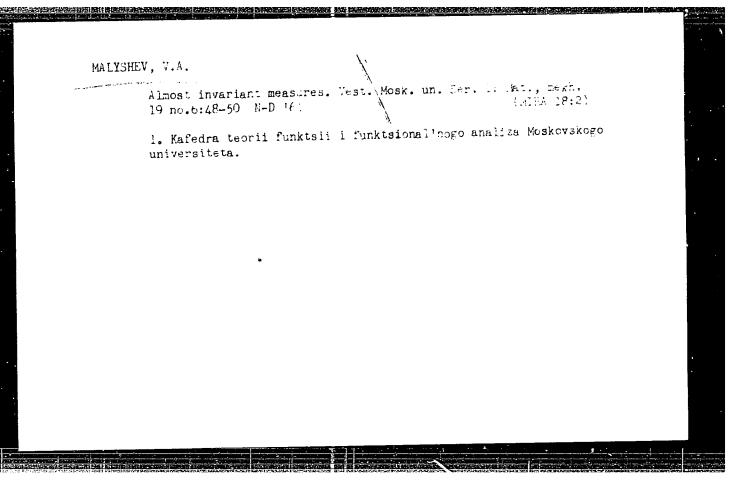
frequency characteristics. Eq.(5) was checked for the case of the photoconductivity of CdS, using as samples industrial photocresistors type \P G-K1 (FS-K1) and \P C-K1 (FS-K2). Experiments showed that the photo-characteristics of these photoresistors were substantially linear within the whole range of values of the light flux. Nowhen plotted as $i \oplus f(\sqrt{N})$. The light beam from a small lamp was modulated mechanically and produced a well defined square wave form. Comparison of the theoretical frequency characteristics with experimental data gave close agreement when σ/σ_1 was plotted against f(x). At low frequencies the experimental points fell below the theoretical curve. This was attributed to the effect of the electron traps in CdS affecting the recombination processes. Hence in the determination of the magnitude of $\sqrt{N}\alpha$ a frequency was chosen at which $\sigma/\sigma_0 = 0.2$. There are 4 figures.

ASSOCIATION: Taganrogskiy radiotekhnicheskiy institut

(Taganrog Radiotechnical Institute)

SUBMITTED: January 3, 1962

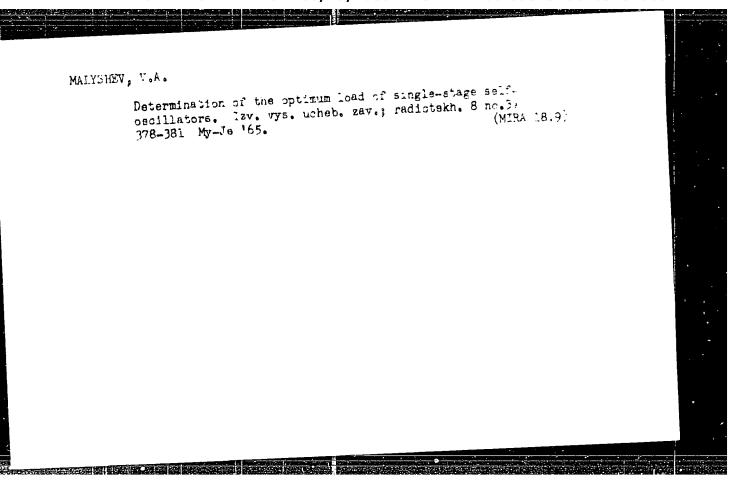
Card 3/3

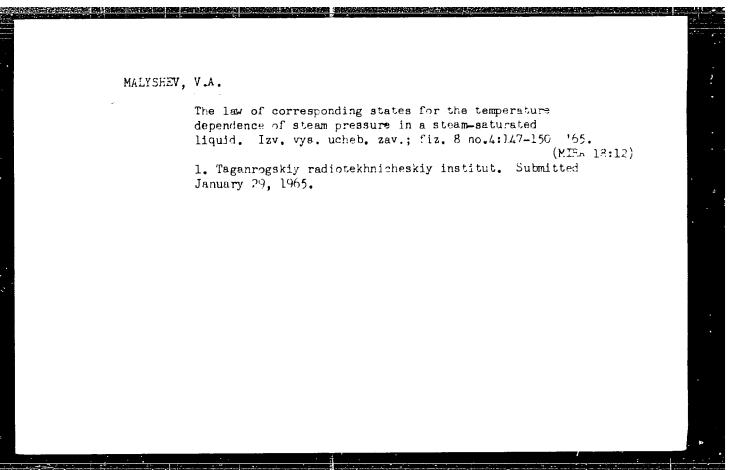


ALEKSANDROV, Nikita Mikhaylovich, kand. med. nauk; KLEMENIOV, Anatoliy Vasil'yevich, kand. med. nauk; MALYSHEV, Vasiliy Alekseyevich, kand. med. nauk, FELKHOVURAYA, N.V., red.

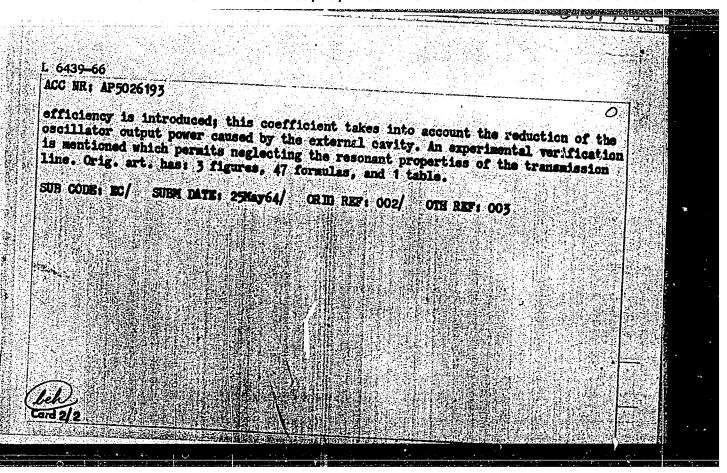
[Emergency storat logical aid] Neotlozhnaia stomatologicheskaia pomoshch'. Leningrad, Meditsina, 1965. 116 p. (MLA 18:6)

MALYSHEV, V.A. Phenomenological theory of one-component diffusion, Izv. vys. ucheb. zav.; fiz. 8 no.2:70.72 '65. (MIRA 18:7) 1. Taganrogskiy radiotekhnicheskiy institut.





L 6439-66 ENT(1)/EWA(h) ACC NR: AP5026193 SOURCE CODE: UR/0142/65/008/004/0411/0419 AUTHOR: Malyshev, V. ORG: none TITLE: Stabilizing the frequency of shf oscillators by connected via a half-wave line SOURCE: IVUZ. Radiotekhnika, v. 8, no. 4, 1965, 411-419 TOPIC TAGS: shf oscillator, frequency stabilization ABSTRACT: Full potentialities of the external-cavity method of shf-oscillator stabilization and the problem of less of the oscillator power caused by its additional load are investigated in the present article which is an outgrowth of some earlier American works (M. Magid, IRE Nat'l Conv. Record, Mar 1957, 1, 208 and others). Frequency stabilization in a shf oscillator whose external cavity is connected via a transmission line of integer-half-waves length is theoretically considered. Formulas are developed for stabilization coefficients depending on the feedback delay and on the external reactive load. A new coefficient of stabilization Card 1/2 UDC: 621.373.52



L 10540-66

ACC NR: AP5022427

SOURCE CODE: UR/0109/65/010/009/1635/1645

AUTHOR: Malyshev, V. A.

36 . B

ORG: none

TITLE: Approximation of the current-voltage characteristic of a tunnel diode by polynomials in a quasi-linear analysis of the diode operation

SOURCE: Radiotekhnika i elektronika, v. 10, no. 9, 1965, 1635-1645

TOPIC TAGS: tunnel diode, current voltage characteristic, electronic amplifier, electronic circuit, electronic oscillator

ABSTRACT: Heretofore, analytical approximations of tunnel-diode I-V

ABSTRACT: Heretofore, analytical approximations of tunnel-diode 1-v characteristics have never permitted a simple and regorous examination of tunnel-diode circuits in a quasi-linear approximation. The present article attempts to solve this problem by representing the diode current as an exponential polynomial of voltages across the diode depletion layer. Formulas for

Card 1/2

UDC: 621.382.233.001

L 10540-66

ACC NR: AP5022427

approximating the I-V curve by general polynomials of the 3rd, 4th, 5th, and 6th degree are developed; an especially simple solution is obtained with the 6th degree polynomial. Also, formulas are derived for the oscillatory characteristic and the negative-resistance phase; these formulas are intended for analyzing the behavior of tunnel-diode oscillators and amplifiers in a quasi-linear approximabehavior. An experimental verification of the formulas is claimed. Orig. art. has: 6 figures and 57 formulas.

SUB CODE: 09 / SUBM DATE: 26 May64 / ORIG REF: 005 / OTH REF: 004

Card 2/2 00

L 10395-66
ACC NR: AP5026901 SOURCE CODE: UR/0109/65/010/010/1814/1823

AUTHOR: Malyshev, V. A.

35 B

ORG: none

TITLE: Investigation of nonlinear characteristics of a complete equivalent circuit of the tunnel diode

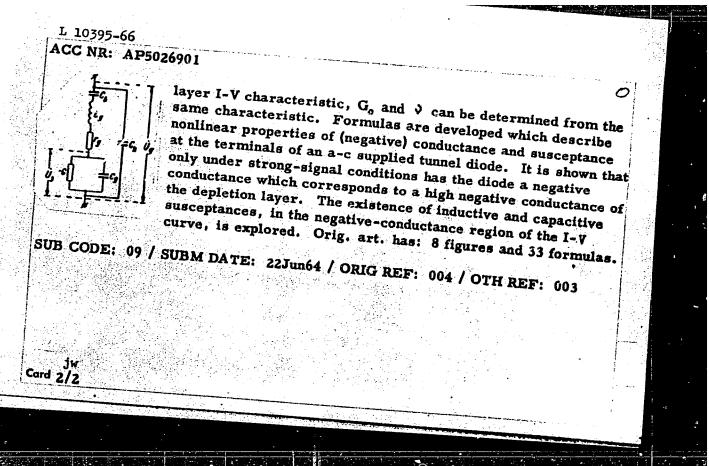
SOURCE: Radiotekhnika i elektronika, v. 10, no. 10, 1965, 1814-1823

TOPIC TAGS: tunnel diode, semiconductor diode

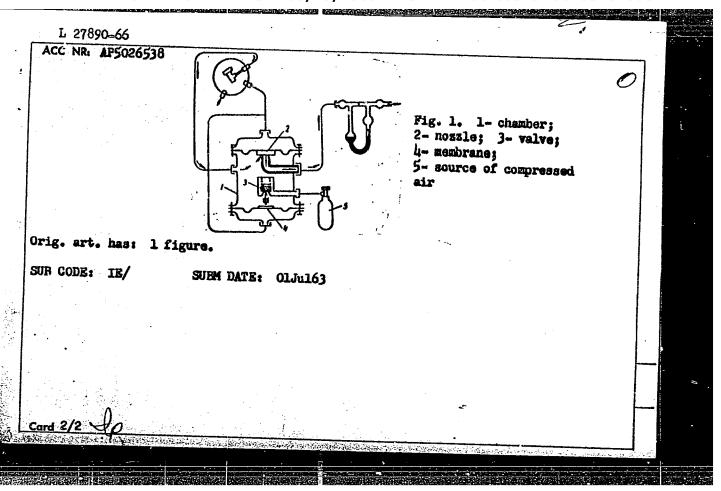
ABSTR : The connection between the parameters of the complete tunnel-diode equivaler circuit (see figure) and the nonlinear characteristics of an equivalent diode a-c admittance is investigated. The depletion-layer negative conductance is assumed to depend on the voltage amplitude A_d across the depletion layer as: $-G = -G_0(1-vX_d^2); \quad X_d = A_d/u_t, \text{ where } u_t \text{ is the valley voltage of the depletion-}$

Card 1/2

UDC: 621.382.233:539.2.012



L 27890-66 ACC NR: AP5026538 SOURCE CODE: UR/0286/65/000/019/0081/0081 AUTHORS: Kitayev, Yu. V.; Simagin, A. V.; Malyshev, V. A. ORG: none TITLE: A device for testing a diving respiratory apparatus? SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 19, 1965, 81 TOPIC TAGS: respirator, pressure regulator, automatic pressure control ABSTRACT: This Author Certificate presents a device for testing a diving respiratory apparatus. The device contains a sensitive element in the form of a membrane dividing the casing into two compartments and directing the flow of a gas stream through a nozzle regulated by a measuring element (see Fig. 1). To broaden the limits of testing pressure without destroying the sensitive element, the nozzle-containing chamber of the device is provided with a valve and an auxiliary membrane which is equal to the effective size of the membrane and which directs the valve. The valve and the auxiliary membrane regulate the pressure delivered by a source of compressed Card VDC: 626.025.001.4



KLOSS, B.M., MALYSHEV, V.A.

Determining the complexity of some classes of furctions.

Vest. Mosk. un. Ser. 1: Mat., mekh. 20 no.4:44-51 Jl-Ag '65.

(MIRA 18-9)

1. Kafedra teoril veroyatnosti Moskovskogo gosudarstvennogo
Universiteta imeni M.V. Lomonosova.

MALYGREV, 7.4.

A.M. Kolmoverov's problem. Vest. Nose. un. Ser. 1: Mat., rekn. 10
no. 0:8-10 M-D '05.

1. Kafedra Laterati therkovo analida Mosvovrsovo universitota.
Submitted Feb. 10, 1964.

<u>L 36196-66</u> SMT(1)

ACC NR: AP6011451 SOURCE CODE: UR/0109/66/011/004/069//0708

AUTHOR: Voloshchenko, Yu. P., Malyshev, V. A.

ORG: none

TITLE: Nonlinear theory of negative-conductance TW amplifiers , .

SOURCE: Radiotekhnika i elektronika, v. 11, no. 4, 1966, 599-765

TOPIC TAGS: TW amplifier, electronic amplifier, austributed amplifier,

amplifier design

ABSTRACT: An attempt is made to construct a nonlinear theory of an amplifiers operating under stationary conditions. Assumptions for a amplifier is designed with nonlinear susceptances as a negative northness conductances, (b) no reflections in the amplifying system, (c) small length, i.e., the amplitude propagation constant is considerably smalls we have

Card 1/2 UDC: 621.385.632.011.222

L 36196-66

ACC NR: AP6011451

phase constant. The method of successive approach closs is used. The troop recented over the case of tunnel-diode TW amplifiers, in the zeroth or first approximations. Tunnel gaps with oscillatory characteristics are a majority which are associated with soft and hard excitation conditions. The reast sobtained for the tunnel-diode amplifier are also applicable to an extended (along the transmission line) reflex klystron that operates at a repeller voltage corresponding to the oscillation-zone center. Two Supplements give details of operation with two integrals used in the article. Originant, has: 2 figures and 76 formulas.

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SUB CODE: 09 / SUBM DATE: 04Jan65 / ORIG REF: 002 / OTH REF: 003

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L 33393-66 EEC(k)-2/EWP(k)/E	WT(1)/FBD/T IJP(c) WG	7		
ACC NR. AP6011461	SOURCE CODE: U/0109/66/011/004/0	767/0,863		
AUTHOR: Malyshev, V. A.		42		
ORG: none		42	,	
TITLE: Quasilinear negative con	nductance of quantum devices			
SOURCE: Radiotekhnika i elektro	onika, v. 11, no. 4, 1966, 767-769	!		
TOPIC TAGS: quantum device, qua	antum generator	:		
ABSTRACT: Formulas are given fo	or the quasilinear negative conductance O o	f three-		
and four-level resonator-type of	quantum devices based on one transition. The			
conductance O in a quasilinear	r approximation is given by: $G_{\epsilon} = -G_{\epsilon} / (1 + X^{2})$;	X = Ar		
	ms for three types of quantum systems, kinet			
	formulas for the parameters $G_{\mathbf{o}}$ and \mathbf{r} , and for purely conductive $G_{\mathbf{o}}$ (when the quantum frequency			
exactly corresponds to the free	quency of energy transition from the i-th legart. has: 9 formulas and 1 table.	vel to	-	
SUB CODE: 10,09 SUBM DATE: 03Dec	c64 / ORIG REF: 003 / OTH REF: 001			
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Card 1/1	UDC: 621.378.3.011.	.222		
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05073-07 IN(F)ING Idl(e) ACC NR. AR6023248

SOURCE CODE: UR/0044/66/000/003/V056/V056

AUTHOR: Malyshev, V. A.

REF SOURCE: Sb. Diskretn. analiz. Vyp. 5. Novosibirsk, 1965, 27-30

TITLE: On the possibility of calculating discrete functions within a certain proba-

SOURCE: Ref. zh. Matematika, Abs. 3V200

TOPIC TAGS: control theory, mathematic analysis

TRANSLATION: The image of a set B_n of binary sequences of length n in B_m is called a discrete (n,m)-function. Let the control system $\mathfrak A$ compute some (n,m)-function ϕ . It is said that (n,m)-function f is p-computed by control system $\mathfrak A$ if the function f and ϕ coincide at least for $[p \cdot 2^n]$ values of the arguments $(0 \cdot p < 1)$. Then schemes of functional elements are considered having two inputs and realizing all functions of two variables. By the complexity of a scheme is meant, as usual, the number of functional elements in it. By L(f,p) is meant the least of the complexities of the schemes which p-compute function f. Let $L(n,m,p) = \max L(f,p)$, where the maximum is taken for all possible (n,m)-functions f. The following is proved: Theorem. If $m(n) \to +\infty$ and

 $\frac{\log_2 m(n)}{\to 0}$ $L(n, m, p) \sim \frac{p \cdot m(n) \cdot 2^n}{n}$ then

Card 1/2

IDC: 519.95

ACC NR: AR602324	3	9
where for any ϵ >	0 the portion of the $(n,m(n))$ -functions for where $L(f, p) < (1-\epsilon) \cdot \frac{p \cdot m(n) \cdot 2^n}{n}$,	hich
approaches zero w	th a growth n. V. Kudryavtsev.	
SUB CODE: 12/	SUBM DATE: none	
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Card 2/2		

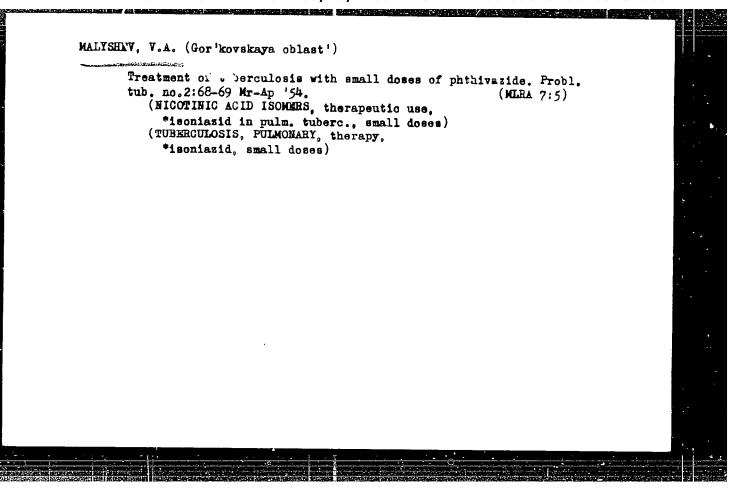
MALYSHEV, V.A., NAZAROVA, Z.Ya.

Some data on anicteric leptospirosis in Chelyabinsk Province. Zhur. mikrobiol., epid.i immun. 33 no.4:62-64 Ap '62.

(MIRA 15:10)

1. Iz Chelyabinskoy oblastnoy sanitarno-epidemiologicheskoy stantsii.

(CHELYABINSK PROVINCE-LEPTOSPIROSIS)



USSR/ Chemistry - Chemical engineering; Industrial Economics FD-2720

Card 1/1

Pub. 50 - 1/20

Author

: Malyshev, V. A.

Title

: Concerning the methods to be used in the calculation of the production capacity of chemical industry enterprises

Periodical

: Khim. prom. No 5, 257-260, Jul-Aug 1955

Abstract

: Continues a discussion begun by M. M. Fedorovich in Khim. prom. No 2, 33, 1953 and No 2, 87, 1954. Expresses the view that the production capacity of plants

Expresses the view that the production capacity of plants should be estimated on the basis of the output of goods of high quality, i.e. of a quality which conforms with GOST standards. Four references, all USSR, all since 1940.

LAVHUKHINA, A.K.; MOSKALEVA, L.P.; MALYSHEV, V.A.; SATAROVA, L.M.;

SU KHUN-GUY [Su Hung-Kusi]

Angular distribution of Ma²⁴ muclei and fission fragments in the interaction of high energy protons with nuclei of gold and uranium. Zhur.eksp.i teor.fiz. no.3:994-995

Mr '60.

1. Institut geokhimii i analiticheskoy khimii Akademii nauk SSSR.

(Sodium--Isotopes) (Protons) (Muclear reactions)

307/130-58-11-7/16

AUTHORS: | Ealyshev, V.A., and Gorbachev, A.F., Engineers, and

Papush, A.G., Candidate of Technical Sciences

Reduction of Metal Claum tion in Cauting Forging Ingets TITLE:

(Umen'sheniye rashkhoda metalla pri otlivke krupnykh

kuznechnykh slitkov)

Card 1/2

FERIODICAL: Metallurg, 1958, Nr 11, p 16 - 18 (USSR)

ABSTRACT: In 1955 electric heating of hot-tops of large carbon and alloy steel ingots was advantageously adopted at the in. Il'icha (im. Il'ich) works. In 1957 the filling of hot tops was increased but further advantage was not obtained. The insulation of the hot top was improved by increasing the thickness of the refractory from 40 to 160 rm (Fig 1), the effectiveness of this being shown with ingots of the effectiveness of this being snown with ingosts and 55 km steels. nominal weights 38 and 54 tornes of 60 kmG and 55 km steels. A third ingot of nominal weight 35.2 tonnes of type 55 a third ingot of nominal weight refractory in but steel was cast with the thickest refractory in but without electric heating of the hot top. The authors without electric heating of the hot top. give details of these ingots (table) and show sulphur prints of the smaller ingots (Fig 2). Study of these has shown that in all the ingots the pipe, porosity and crude segregation were above the body of the ingot.

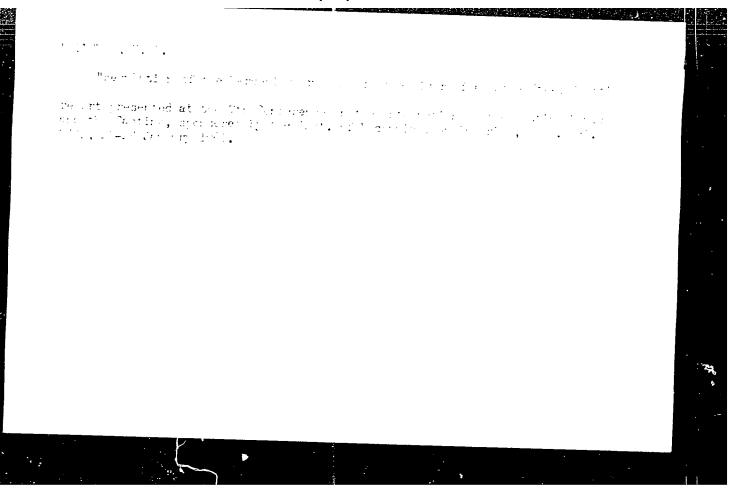
CIA-RDP86-00513R001032010002-2" APPROVED FOR RELEASE: 06/20/2000

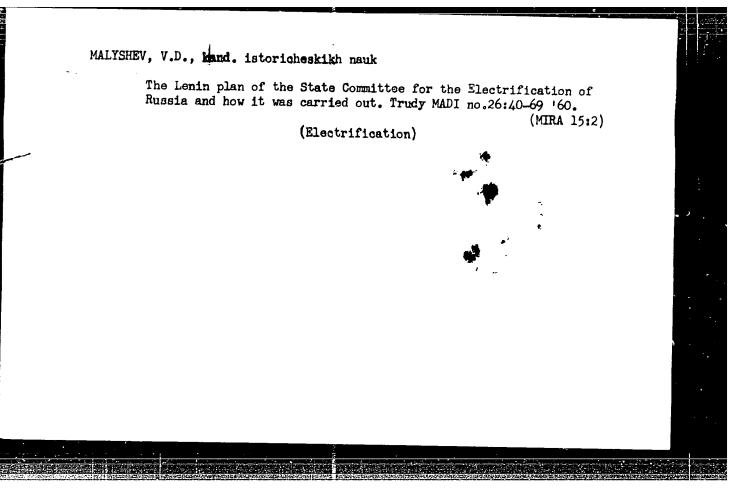
Reduction of Metal Consumption in Casting Forging Ingots

Four further ingots were cast with electrical hot top heating: no effect of the changed hot-top configuration on stripping was observed. Joint tests with the Shdanovs-kiy metallurgical institute showed that the quality of the metal had not suffered through the considerable reduction in the hot top volume.

There are 2 figures and 1 table.

Card 2/2





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KLIMKOVICH, I.G., MALYSHKV, V.D.
               Tracheobronchoscopy using anesthesia and muscle relaxants; preliminary
               report [with summary in English]. Khirurgiia 34 no.6:78-83 Je '58
                                                                (MIRA 11:8)
               1. Is 4-y kafedry klinicheskoy khirurgii (zav. - prof. V.I. Kazanskiy)
               TSentral'nogo instituta usovershenstvovaniya vrachey na baze TSentral'
               noy klinicheskoybol'nitsy (nach. V.N. Zakharchenko) Ministerva putey
               soobshcheniya.
                       (BRONCHOSCOPY, anesthesia & analgesia
                            anesth. with added musc. relaxants, technic & results
                            (Rus))
                       (ANESTHESIA.
                            in bronchescopy, added use of musc. relaxants (Rus))
                       (MUSCLE RELAXANTS, therapeutic use
                           adjuvant in anesth, for bronchoscopy, technic & results
                           (Rus))
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MALYSHEV, V.D.

Hemodynamics in potentiated anesthesia. Akt. vop. obezbol. no.2: (MIRA 14:5)

l. Iz 4-y kafedry khirurgii (qav. - prof. V.I.Kazanskiy) TSentral'nogo instituta usovershenstvovaniya vrachey na baze TSentral'noy klinicheskoy bol'nitsy Ministerstva putey soobshcheniya (nachal'nik - zasluzhennyy vrach RSFSR V.N.Zakharchenko).

(ANESTHESIA) (BLOOD)

MAKARENKO, T.P., prof.; MALYSHEV, V.D.

Intra-arterial injection of blood as a method of controlling hemodynamic disorders in potentiated anesthesia. Akt. vop. obezbol. no.2:165-170 '59. (MIRA 14:5)

l. Iz 4-y kafedry khirurgii (zaveduyushchiy - prof. V.I.Kazanskiy)
TSentral'nogo instituta usovershenstvavaniya vrachey na baze
TSentral'nog klinicheskoy bol'nitsy Ministerstva putey soobshcheniya
(nachal'nik V.M.Zakharchenko).

(INJECTIONS, INTRA-ARTERIAL)

(BLOOD AS FOOD OR MEDICINE)

(ANESTHESIA—COMPLICATIONS AND SEQUELAE)

(BLOOD—CIRCULATION, DISORDERS OF)

MALYSHEV, V. D., CAND MED SCI, "MATERIAL FOR STUDY OF HEMODYNAMICS IN OPERATIONS UNDER VARIOUS FORMS OF ANESTHESIA." MOSCOW, 1960. (MIN OF HEALTH USSR, CENTRAL INST OF ADVANCED TRAINING OF PHYSICIANS). (KL, 2-61, 218).

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1. IV kafedra khirurgii (zav. prof. V.I.Kazanskiy) TSentral'nogo instituta usovershenstvovaniya vrachey.
(HYPOTHERMIA) (BLOOD__CIRCULATION)

THE RESERVE OF THE PROPERTY OF

MAKAHENKO, T.P., prof.; MALYSHEV, V.D.

Features of hemodynamics during anesthesia. Khirurgiia 36 no.10: 107-112 0 *60. (MIRA 13:11)

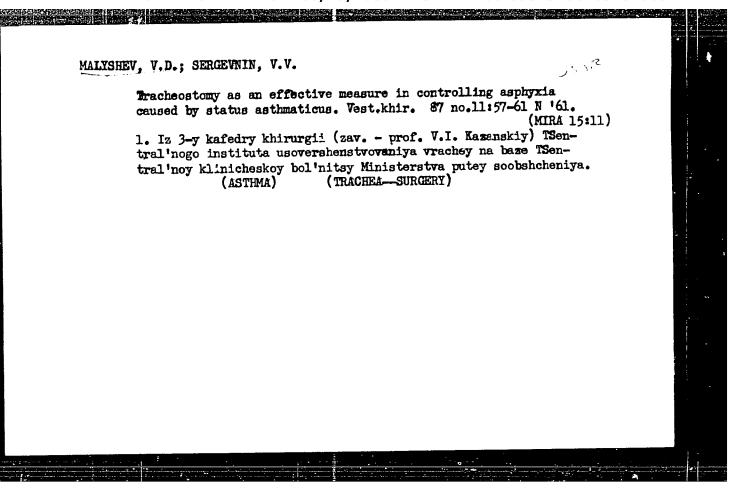
1. Iz 3-y kafedry khirurgii (zav. - prof. V.I. Kazanskiy) TSentral'nogo instituta usovershenstvovaniya vrachey na baze TSentral'noy
klinicheskoy bol'nitsy Ministerstvo putey soobshcheniya (nach. zasluzhennyy vrach RSFSR V.N. Zakharchenko).
(BLOOD-CIRCULATION) (ANISTHESIA)

MAKARENKO, T.P., prof.; SERCEVNIN, V.V.; MALYSHEV, V.D.

Principal problems of anesthesia in patients with functional disorders of the liver. Khirurgiia no.11:20-28 '61.

1. Iz 3-y kafedry khirurgii (zav. - prof. V.I. Kazanskiy)
TSentral'nog' instituta usovershenstvovaniya vrachey na baze
TSentral'noy klinicheskoy bol'nitsy (nach. - zasluzhennyy vrach RSFSR V.N. Zakharchenko) Ministerstva putey soobsheheniya.

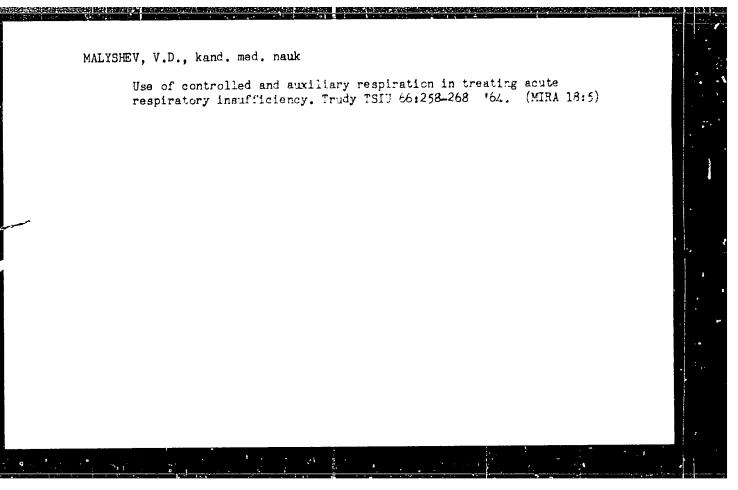
(ANESTHESIA) (LIVER--DISEASES)



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Changes in external respiration depending on the type of anesthesia. Trudy TSIU 59:47-61 '63. (MIRA 17:9)

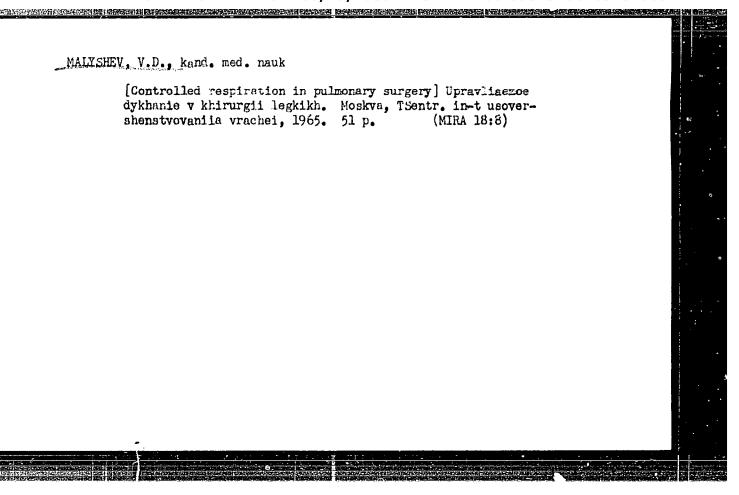
1. II kafedra khirurgii (zav.- prof. B.K. Osipov) TSentral'nogo instituta usovershenstvovaniya vrachey.

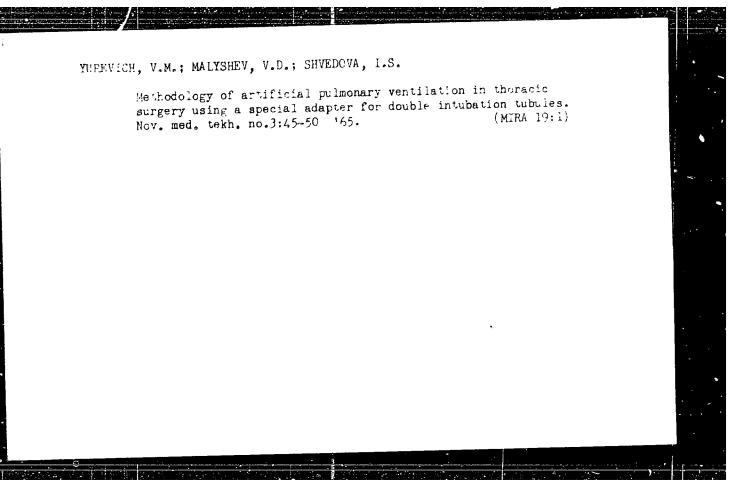


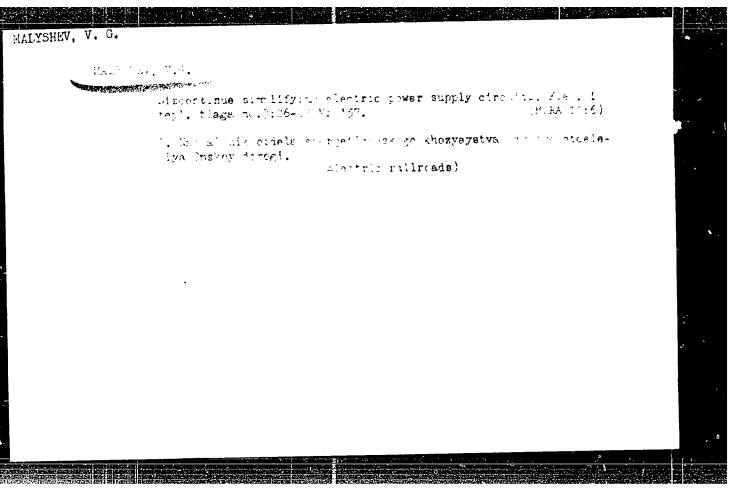
OSIPOV, B.K., prof.; MALYSHEV, V.D., ksmi. med. rauk; YCLEVICE, V.W., kand. med. nauk; GUTKINA, Z.L.; GUEKGV, S.A.

Use of the artificial cough machine IX-rV in sorrica. Practice. Khirurgiia 40 no.7:49-55 Jl 164.

1. 2-ya kafedra klinicheskoy khirurgii (zav. - prof. B.K. (sipov), kafedra rentgenologii (zav. - prof. Yu.N. Sokolov) TSentral'nogo instituta usovershenstvovaniya vrachey i Vsesoyuznyy nauchno-issledovatel'skiy institut meditsinskiykh instrumentov i oborudovaniya (dir. - I.P. Smirnov), Moskva.







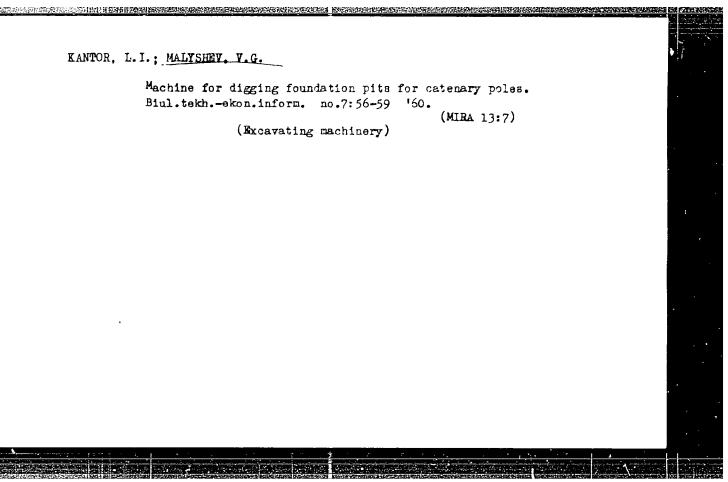
NATIONAL COMMENSATION OF THE RESIDENCE OF THE STATE OF TH

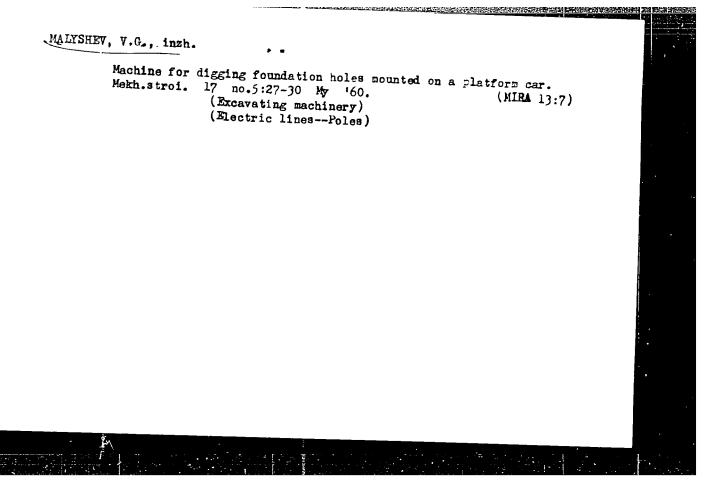
MALYSHEV, V.G., inzh.; MAMONTOVSKIY, V.A., inzh.; PFUL', B.Ye., inzh., red.

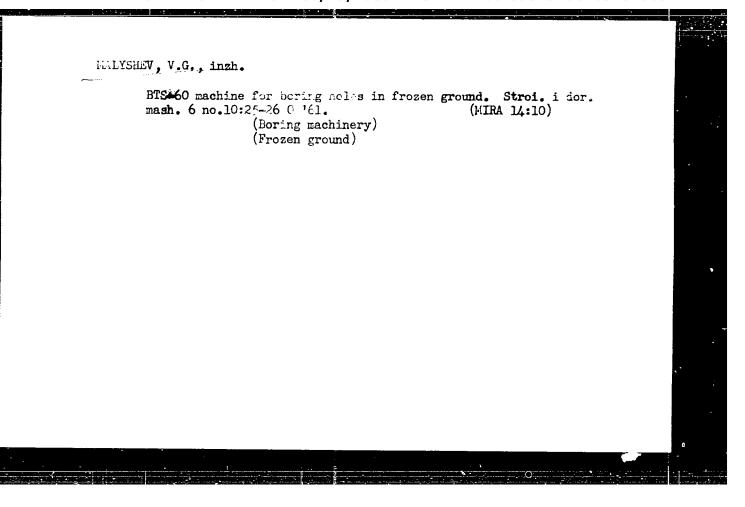
[Machine for boring holes in frozen ground] Mashina dlia bureniia shpurov v merzlykh gruntakh; po materialam PKB Glavstroimekhanizatsii Ministerstva transportnogo stroitel'stva SSSR. Moskva, Gosstroiizdat, 1960. 6 p. (MIRA 14:11)

1. Akademiya stroitel'stva i arkhitektury SSSR. Institut organizatsii, mekhanizatsii i tekhnicheskoy pomoshchi stroitel'stva.Byuro tekhnicheskoy informatsii. 2. Proyektno-konstruktorskoye byuro Glavnogo upravleniya po mekhanizatsii stroitel'nykh rabot Ministerstva transportnogo stroitel'stva SSSR (for Malyshev, Mamontovskiy).

(Boring machinery) (Frozen ground)





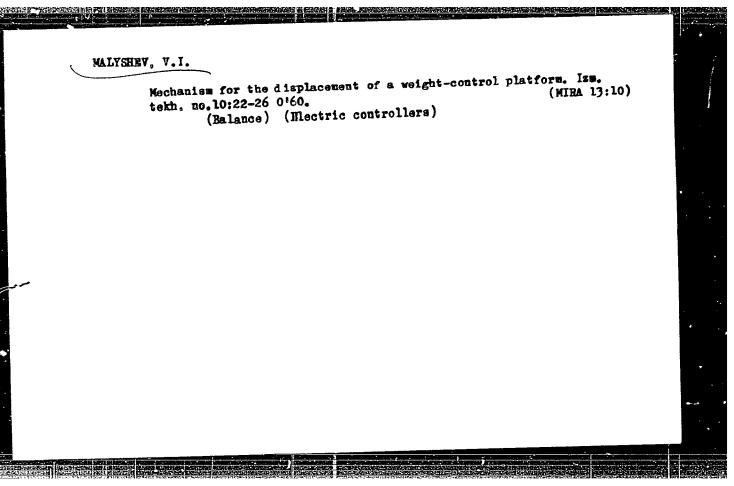


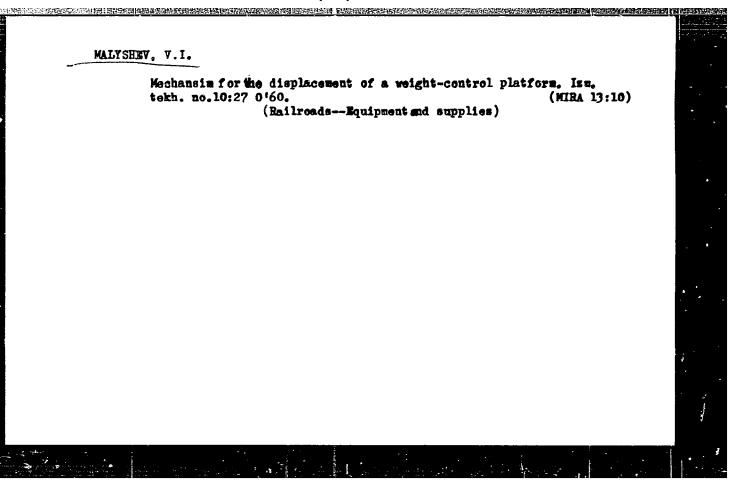
MALYSHEV VII

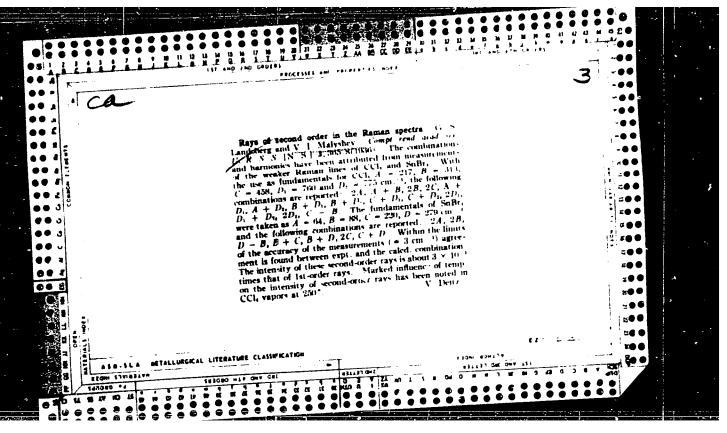
Determination of coefficients of readiactive equilibrium as a method for studying the migration of uranium, ionium, and radium [with summary in English]. Sov.geol. 1 no.7:138-147 Jl. 58.

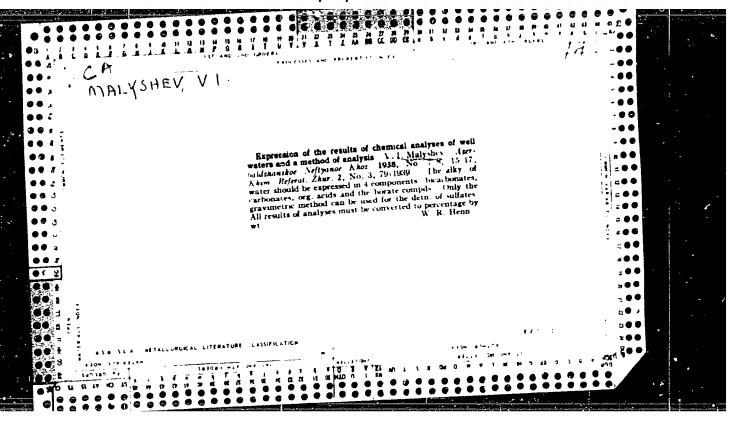
(MIRA 11:11)

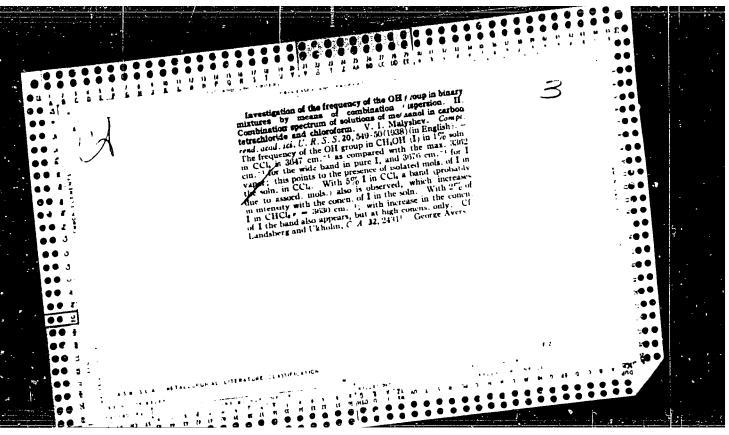
1. Vsesoyuznyy institut mineralinogo syriya.
(Radioactive substances)

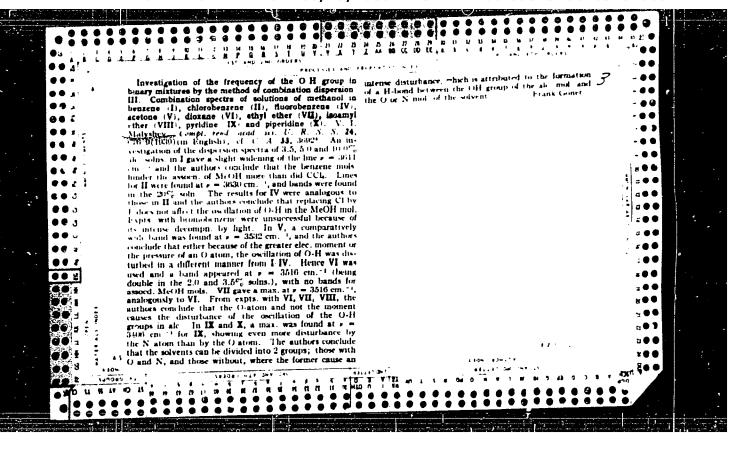


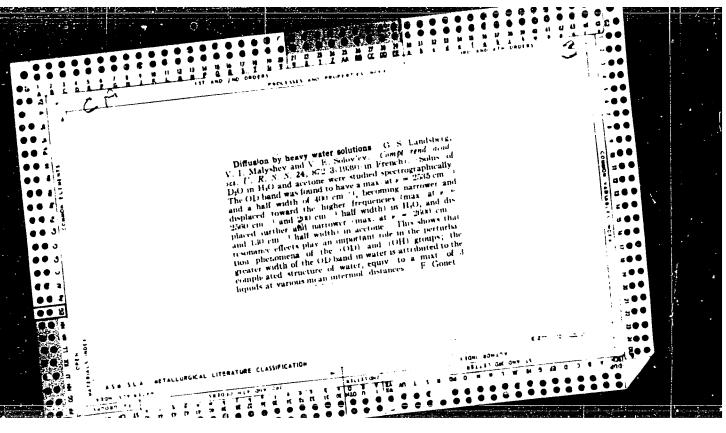


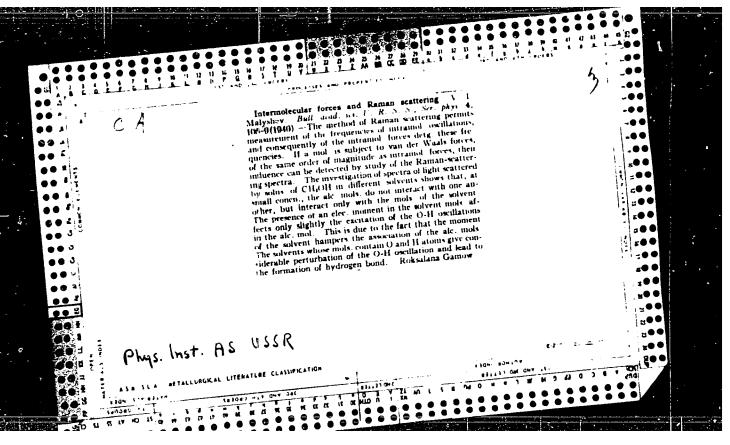


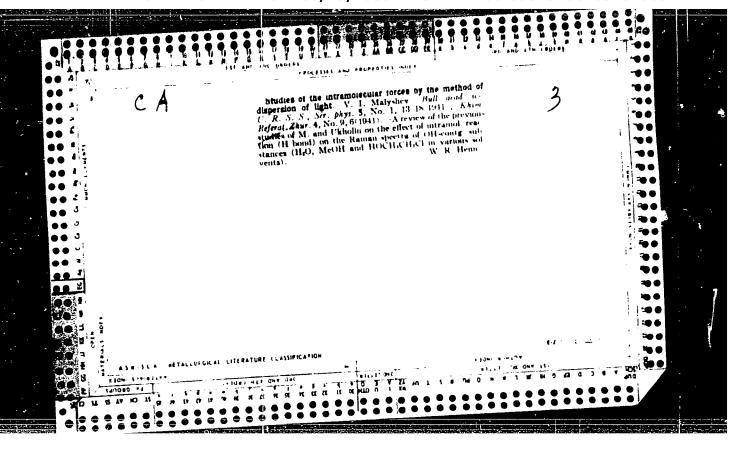


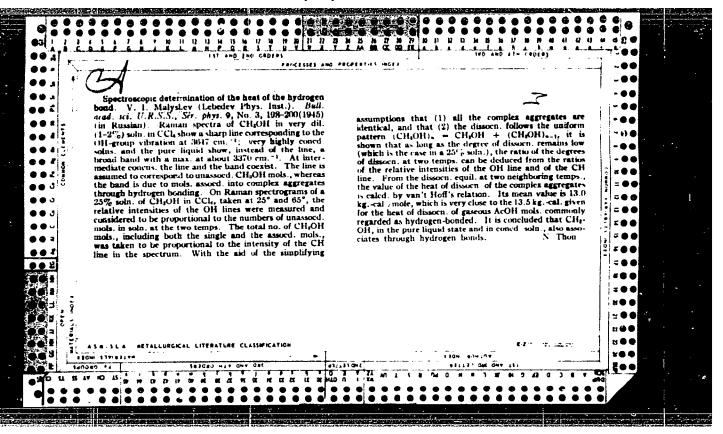












USSR/Chemistry - Hydrogen Bond Chemistry - Dispersion

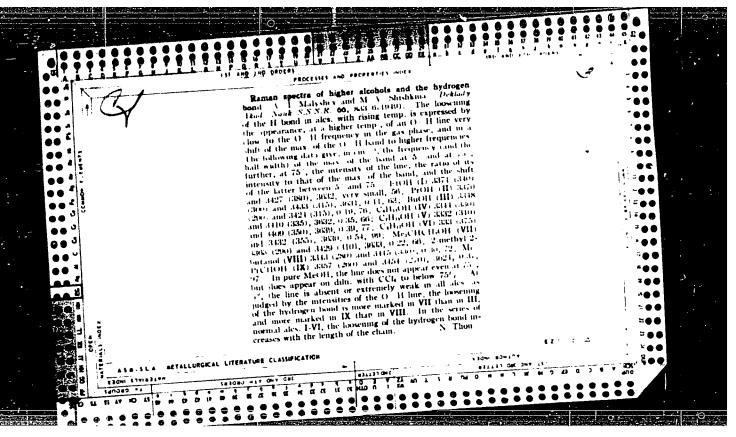
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"Combination Dispersion of Light in Higher Alchhols and the Problem of the Hydrogen Bonds, " V. I. Malyshev, Shishkina, Phys In st ineni P.N. Lebedev, Acad Sci USSR, 3 3/4pp

"Dok Ak Nauk SSSR" Vol LXIV, No 5

Studies combination dispersion spectra of ten monatomic alcohols from methyl to octyl alcohol for various temperatures. Tabulates results. Submitted by Acad G. S. Lendsberg,

PA 50/49T26



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MALYSHEV, V. I.

PA 170 T96

USSR/Physics - Spectroscopy

Nov/Dec 50

"Methods for Increasing the Dispersion of the Spectral Apparatus," V. I. Malyshev, Phys Inst imeni Lebedev, Acad Sci USSR

"Iz Ak Nauk SSSR, Ser Fiz" Vol XIV, No 6, pp 746-752

Author was assisted in the experiments by I. I. Sobel'man, and was guided by advice of G. S. Landsberg. Describes method for triple passage of rays through prism of dispersive system.

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